

**REPORT DOCUMENTATION PAGE**Form Approved  
OMB No. 0704-0188

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**1. REPORT DATE (DD-MM-YYYY)**

16-12-02

**2. REPORT TYPE**

Viewgraph Presentation

**3. DATES COVERED (From - To)****4. TITLE AND SUBTITLE**

Three-Dimensional Simulations of a Gas/Gas, Hydrogen/Oxygen Engine

**5a. CONTRACT NUMBER****5b. GRANT NUMBER****5c. PROGRAM ELEMENT NUMBER****6. AUTHOR(S)**Mark R. Archambault<sup>1</sup>Oshin Peroomian<sup>2</sup>**5d. PROJECT NUMBER**

3058

**5e. TASK NUMBER**

RF9A

**5f. WORK UNIT NUMBER****7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)**<sup>1</sup>Air Force Research Laboratory (AFMC)

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**8. PERFORMING ORGANIZATION  
REPORT NUMBER**

AFRL-PR-ED-VG-2002-310

**9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)**

Air Force Research Laboratory (AFMC)

AFRL/PRS

5 Pollux Drive

Edwards AFB CA 93524-7048

**10. SPONSOR/MONITOR'S  
ACRONYM(S)****11. SPONSOR/MONITOR'S  
NUMBER(S)**

AFRL-PR-ED-VG-2002-310

**12. DISTRIBUTION / AVAILABILITY STATEMENT**

Approved for public release; distribution unlimited.

**13. SUPPLEMENTARY NOTES****14. ABSTRACT**

20030227 155

**15. SUBJECT TERMS****16. SECURITY CLASSIFICATION OF:****a. REPORT**

Unclassified

**b. ABSTRACT**

Unclassified

**c. THIS PAGE**

Unclassified

**17. LIMITATION  
OF ABSTRACT**

A

**18. NUMBER  
OF PAGES****19a. NAME OF RESPONSIBLE  
PERSON**

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(include area code)**

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DTS

3058 RF9A

MEMORANDUM FOR PRS (In-House/Contractor Publication)

FROM: PROI (STINFO)

16 Dec 2002

SUBJECT: Authorization for Release of Technical Information, Control Number: **AFRL-PR-ED-VG-2002-310**  
Archambault, Mark R.; Perroomian, Oshin (Metacomp Technologies, Inc.), "Three-Dimensional  
Simulations of a Gas/Gas Hydrogen/Oxygen Engine" (Viewgraphs)

41<sup>st</sup> AIAA Aerospace Sciences Meeting & Exhibit  
(Reno, NV, 6-9 Jan 2003) (Deadline: 5 Jan 2003)

(Statement A)

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# Three-Dimensional Simulations of a Gas/Gas, Hydrogen/Oxygen Engine

6 January 03



**Mark Archambault**  
Propulsion Directorate  
Space and Missile Propulsion Division  
Air Force Research Laboratory

**Oshin Peroomian**  
Metacomp Technologies, Inc.



# Objective



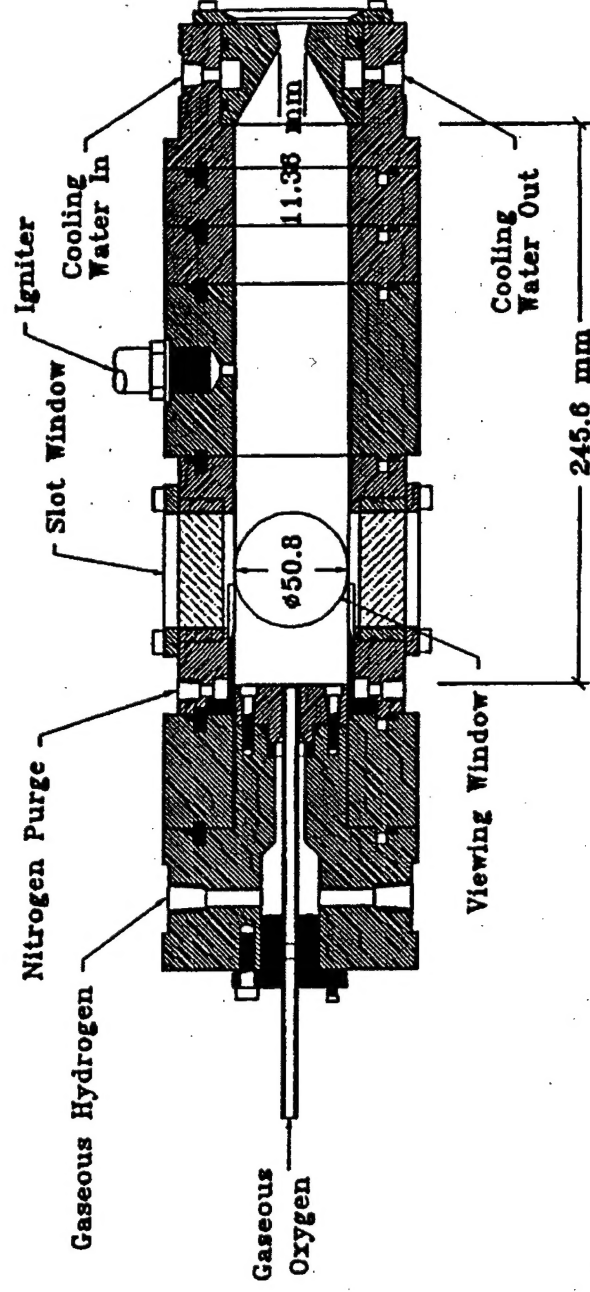
- Develop design tools and methodologies for rocket injectors.
- Use experimental measurements to develop and anchor state-of-the-art flow codes.
- Determine level of fidelity required to reasonably reproduce the essential physical behavior of a coaxial gas/gas injector flow.



# Previous Work



- Experiments — Penn State
  - OH-radical imaging
  - Velocity & species field measurements



from Foust, M.J., Deshpande, M., Pal, S., Ni, T., Merkel, C.L., & Santoro, R.J., "Experimental And Analytical Characterization of a Shear Coaxial Combusting  $\text{GO}_2/\text{GH}_2$  Flowfield," AIAA 96-0646, AIAA 34<sup>th</sup> Aerospace Sciences Meeting & Exhibit, Reno, NV, Jan. 1996.



## Previous Work

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- Computational Modeling
  - DLR (AS3D)
    - 2<sup>nd</sup>-order explicit FV
  - MSFC (FDNS)
    - 3<sup>rd</sup>-order pressure-based predictor/multi-corrector
  - Penn State
    - 1<sup>st</sup>-order preconditioned, coupled, implicit, time-marching
  - AFRL
    - 2<sup>nd</sup>-order preconditioned, coupled, implicit, dual-time stepping. Steady and time-accurate.



# Current AFRL Modeling Effort



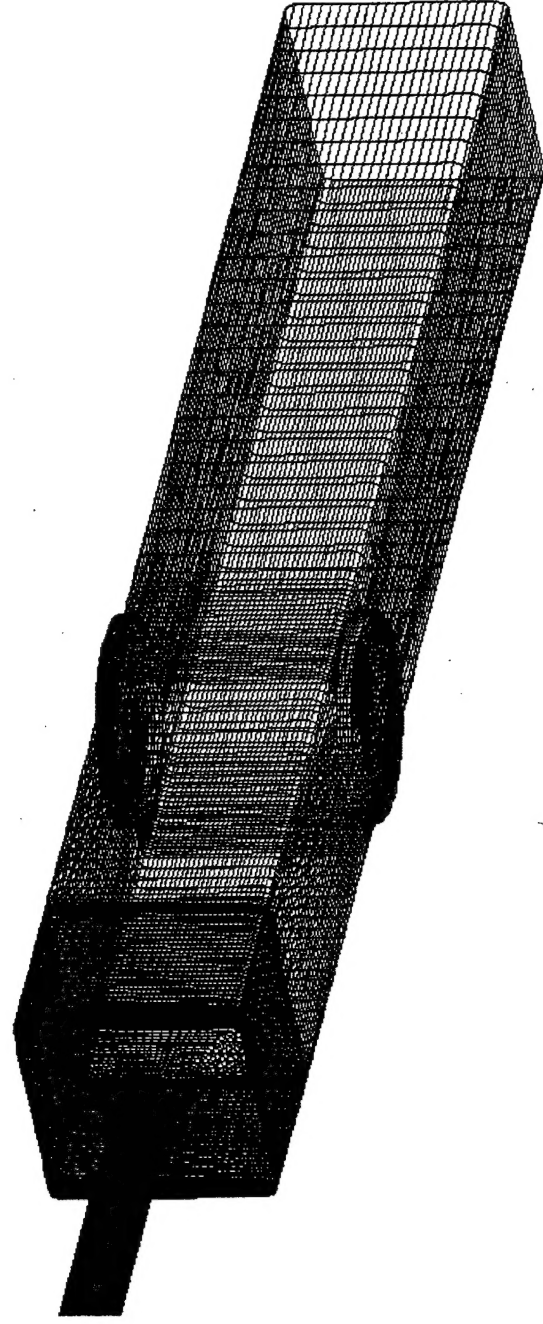
- CFD++ from Metacomp Technologies
  - RANS, LES, hybrid RANS/LES
  - Compressible with high- and low-speed capability
  - Finite rate & equilibrium chemistry
  - 3D structured & unstructured grids
  - Explicit (RK) and Implicit schemes
  - Steady & Unsteady
  - Preconditioning
  - Parallel



# Current AFRL Modeling Effort



- Single-element, shear-coaxial,  $H_2/O_2$  engine
- Refined grid resolution
- Steady & transient 3-D solutions
- Nitrogen curtain purge
- Prelude to multi-element analyses



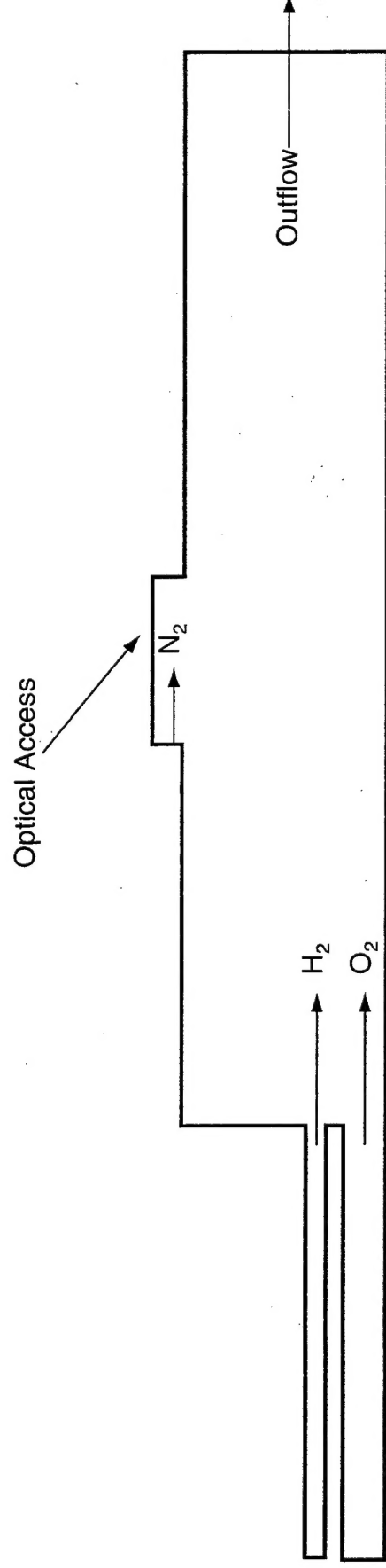




# Current Computational Effort



- Flow conditions
  - $O_2$  mass flow rate: 0.042 kg/s (0.1 lbm/s)
  - $H_2$  mass flow rate: 0.0103 kg/s (0.025 lbm/s)
  - $N_2$  mass flow rate: 0.01 kg/s (0.022 lbm/s)
  - Chamber pressure: 1.29 MPa
  - Inlet temperature: 297K
  - Laminar inlet flow, turbulence allowed to develop

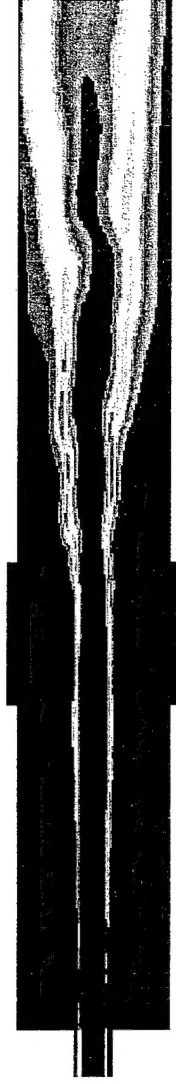




# Current AFRL Modeling Effort



**3-D Steady**



**3-D Instantaneous**



**3-D Time-average**



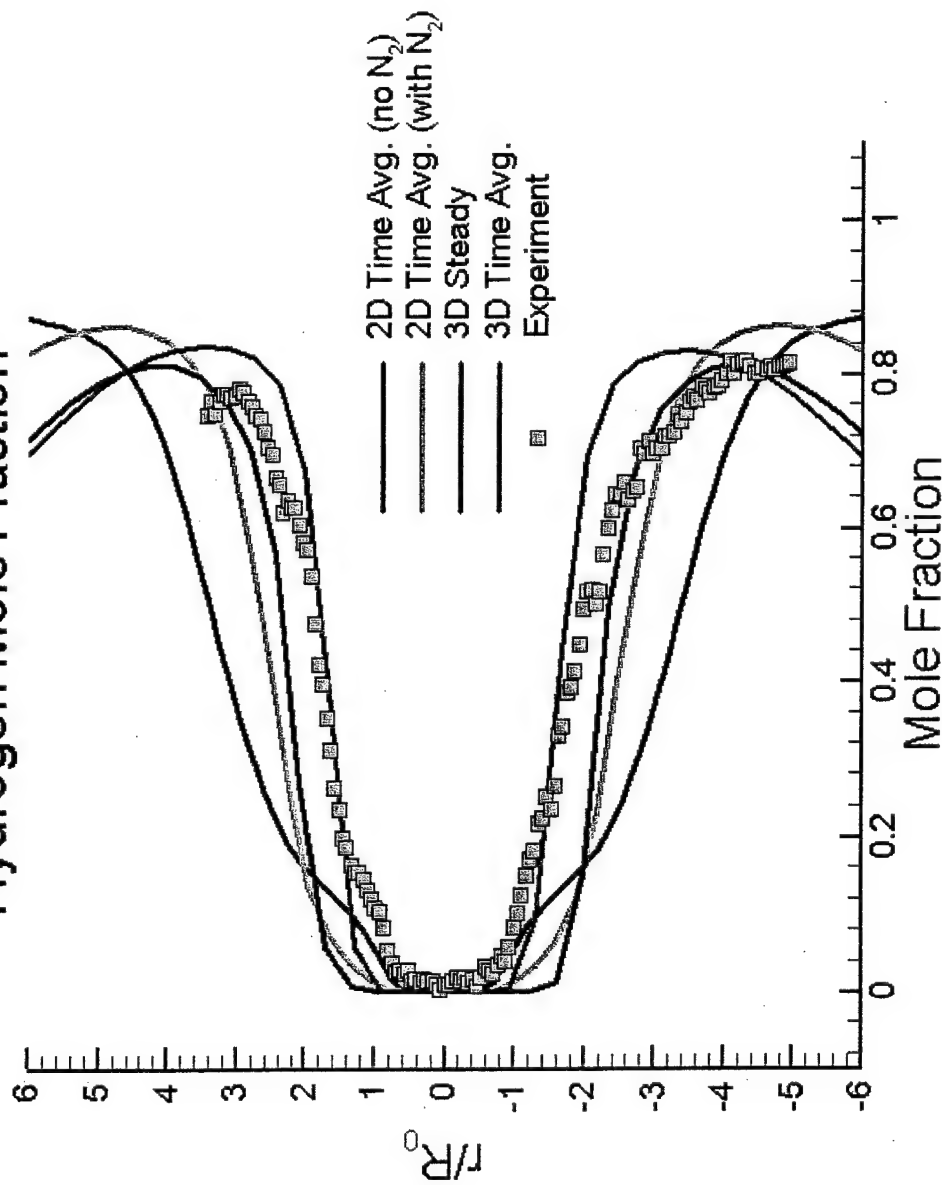
**2-D Time-average**



# Current AFRL Modeling Effort



Hydrogen Mole Fraction



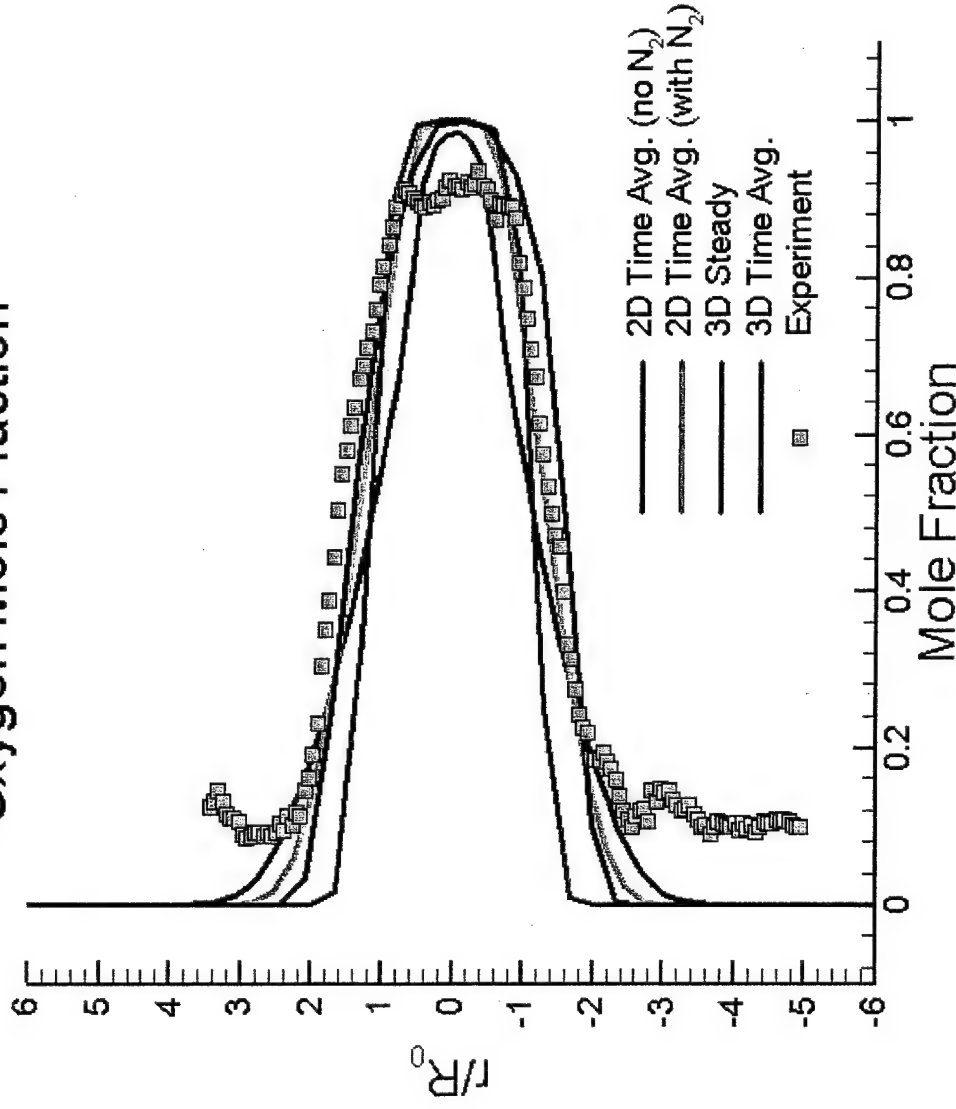
- Comparisons of level of modeling fidelity.
- 3D Time-avg. appears to provide best representation of data.
- No experimental uncertainties on data.



# Current AFRL Modeling Effort



Oxygen Mole Fraction



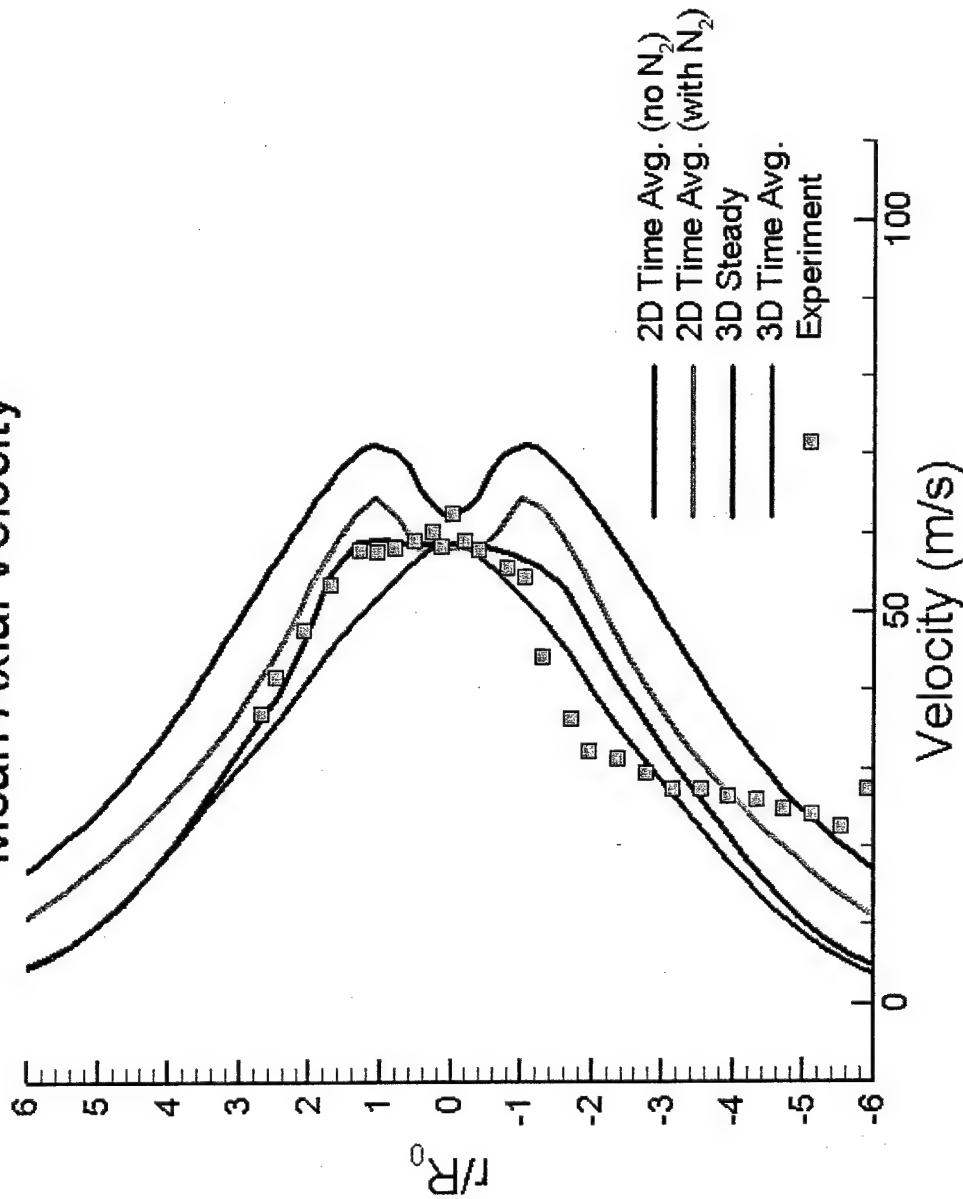
- Comparisons of level of modeling fidelity.
- Quantitatively similar profiles.
- 3D Time-avg. calculation deviates from data in outer part of shear layer possibly caused by flapping of actual flame.



# Current AFRL Modeling Effort



Mean Axial Velocity



- 3D results do not predict peaks in the velocity profile from the greater injection velocity of the hydrogen

- Differences are likely due to the three-dimensional chamber geometry.

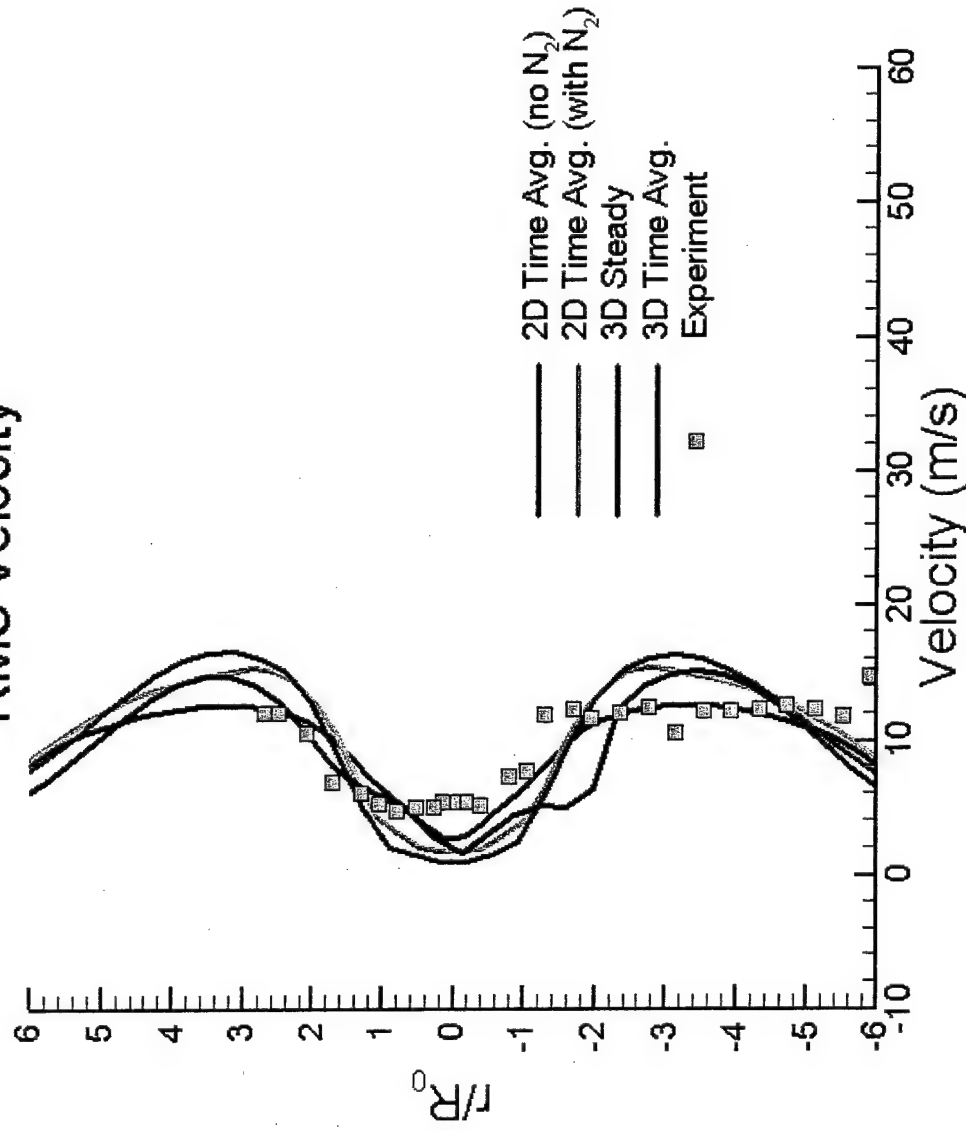
AFRL  
AFRICAN RESEARCH LABORATORY  
AFRL



# Current AFRL Modeling Effort



RMS Velocity



- Calculations are quantitatively similar.
- Appears that RMS velocities are a strong function of turbulence model, but not very sensitive to the degree of fidelity.



# Nitrogen Curtain Purge



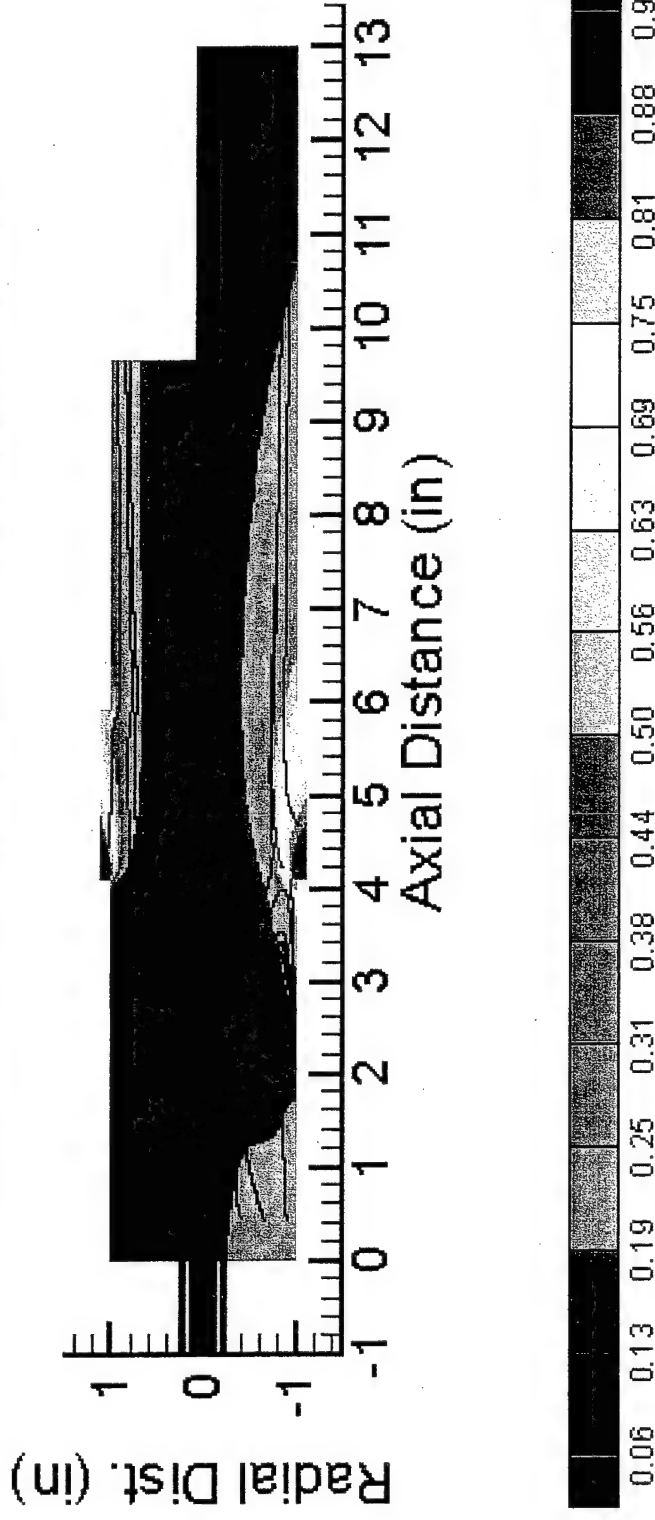
- Experimental feature used to cool optical access
  - Not likely to be in actual flight hardware
- Often neglected by modelers
  - Can result in deviation from experimental data in vicinity of wall
- In 2-D case, the windows are assumed to be axisymmetric. In 3-D case, the windows are located on top and bottom of chamber.



# Nitrogen Curtain Purge



## Contours of Nitrogen Concentration



- 2-D (top half) compared with 3-D (bottom half).
- Slight shift forward of upstream recirculation zone in 3-D.
- Nitrogen being entrained upstream in 3-D case.

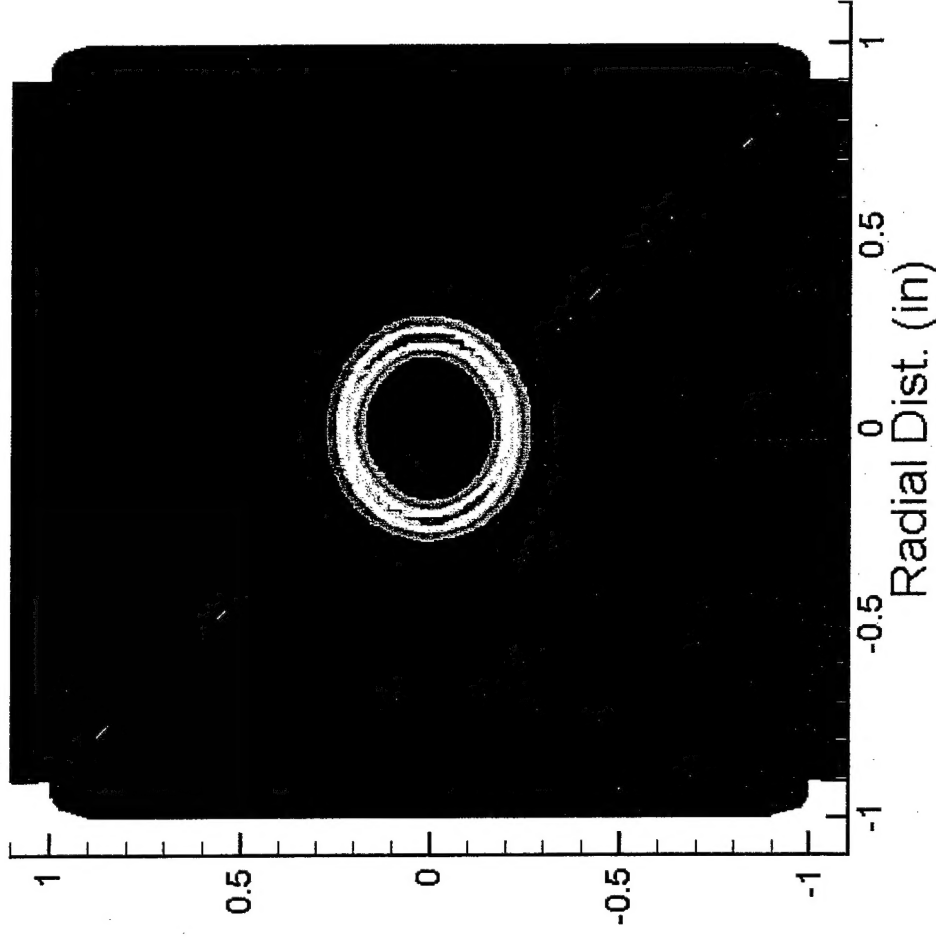




## Current AFRL Modeling Effort

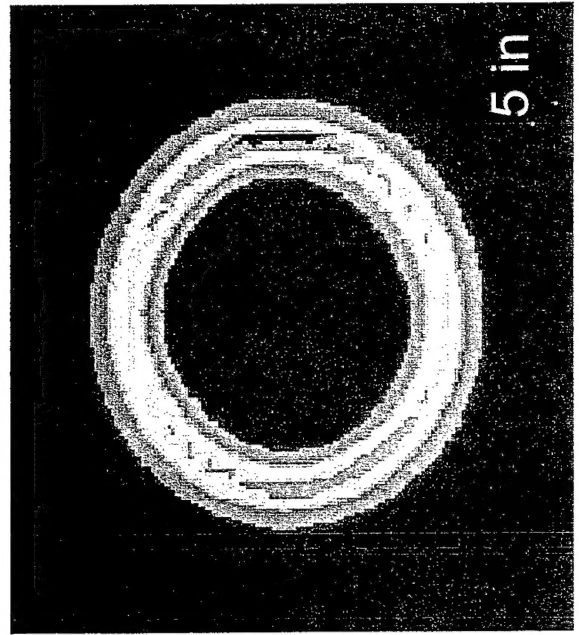
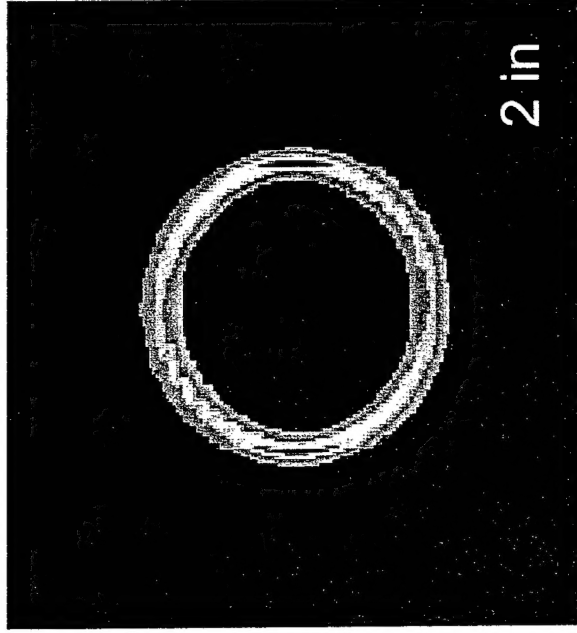
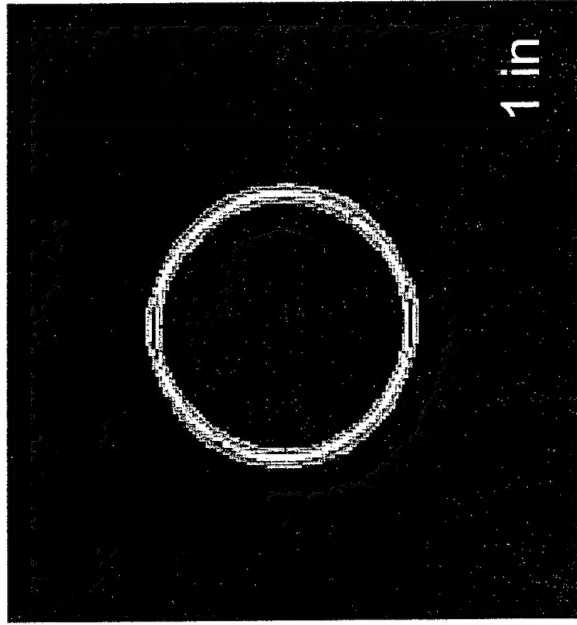
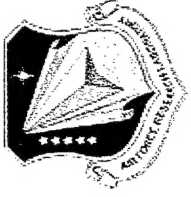


- No obvious three-dimensional patterns (such as helical structures) found.
- Slight variations in azimuthal direction can be attributed to the presence of the nitrogen purge.
- Suggests that planar or wedge symmetry could be used in future calculations.





# Current AFRL Modeling Effort



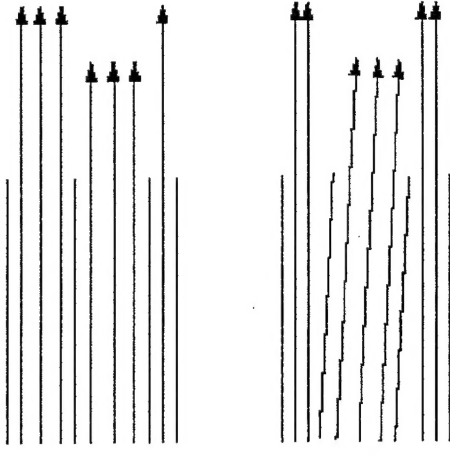
- Measurement indicates distance from injector.
- Streamtraces and contour plots do not indicate any temporal spatial changes in azimuthal direction.



# Follow-On Plans



- Fully three-dimensional calculations
  - Oxygen Post Biasing
  - Off-axis parallel streams
  - Non-parallel streams
  - Multi-element injectors
  - Hydrocarbon
- Trend Analysis
  - Scalability





# Summary and Conclusions



- Results indicate a marked difference between steady and time-accurate results. 3-D calculations seemed to predict the data as well as or better than 2-D calculations.
- A comparison between 2-D and 3-D models of the nitrogen purge showed differences that could be important when relying on CFD to design experiments.
- No evidence of 3-D patterns found in shear layer. Suggests that planar or wedge symmetry may be sufficient for future calculations.
- 3-D results are preliminary. Need to continue learning how to compute these types of flows to fully understand how to model this class of problems.